OAI Fiber Reinforcement Architectures of PMCs on the Hygrothermal-Mechanical Performance for Aeropropulsion Applications

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ABSTRACT

A rigid lightweight sandwich support structure, for the combustor chamber of a new generation liquid propellant rocket engine, was designed and fabricated using PMC facesheet on a Ti honeycomb or Carbon foam core. The facesheet consisted of high stiffness carbon fiber, M40JB, and high temperature Polyimides, such as PMR-II-50 and HFPE-II. Six different fiber architectures; 4HS woven fabric, uni-fabric, woven-uni hybrid, stitched woven fabric, stitched uni-fabric and tri-axial braided structures have been investigated for optimum stiffness-thickness-weight-performance design criteria for the hygrothermal-mechanical propulsion service exposure conditions including rapid heating up to 200°F/sec, maximum operating temperature of 600°F, internal pressure up to 100psi.

An extensive property and performance database including dry-wet mechanical properties at both 25°F and 600°F in various loading modes, thermal and physical properties including blistering onset condition was developed for fiber architecture down-selection and design guidelines. Various optimized process methods including vacuum bag compression molding, solvent assistant RTM (SaRTM), resin film infusion (RFI) were utilized for PMC panel fabrication depending on the architecture type. In the case of stitched woven fabric architecture, the optimal stitch pattern was chosen in terms of stitch density and yarn size, based on both in-plane mechanical properties and blistering performance. Potential reduction of the in-plane properties transverse to the line of stitching was also evaluated. Attempt to correlate the experimental results with theoretical micro-mechanics predictions will be presented.





SUBJECT MATTER

- □ Parent HOTPC Program
 - Technical Program Overview & Strategies
- ☐ Fiber Architecture Studies
 - Objectives and Work Plans
 - Materials and Processing
 - Current Status and Results
 - > Stitching Optimization/Evaluation
 - Composite properties/performance
- Summary and Conclusion
- ☐ Continuing Work Plans



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HOTPC PROGRAM SYNOPSIS

Objective:

Evaluate and develop carbon fiber reinforced high temperature polymer matrix composite (PMC) materials and fabrication technology suitable for manifolds, thrust chamber backup supports & attachments or turbo-pump housings in a new generation rocket engine.

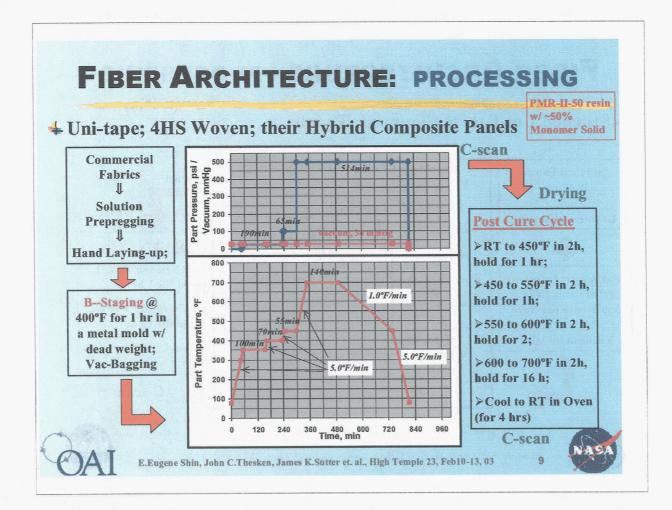
Values:

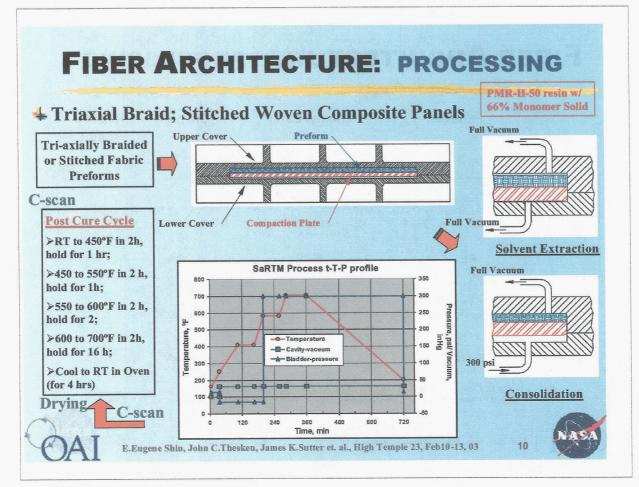
- ☐ Significant weight reduction by replacing metal/ceramic components with PMC
- ☐ Increased thrust-to-weight ratio, reduced fuel consumption, thus cost saving
- Utilization of current enabling technologies in materials, design, process and fabrication areas, i.e., high feasibility!

Challenge:

- Needed high thrust-to-weight ratio (>30:1) that must be achieved to make this a viable flight propulsion system. By component weight reductions up to 25-30%,
- Required high stiffness (less than 0.05" deflection in a 12"×12" panel) and high temperature capabilities up to 600°F,
- Required good hygro-thermal stability especially under rapid heat-up exposure up to 200°F/sec



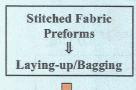




FIBER ARCHITECTURE: PROCESSING

♦ Stitched Uni-Fabric Composite Panels

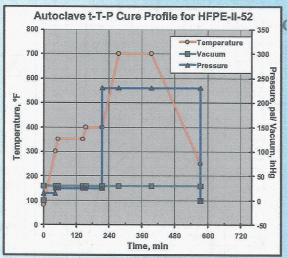
HFPE-II-52 resin





Vacuum Bagging







Post Cure Cycle

- >RT to 450°F in 1h, hold for 1 hr;
- >450 to 700°F in 6h, hold for 16 h:
- > Cool to RT in Oven (for 4 hrs)

C-scan



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FIBER ARCHITECTURE: PROCESSING

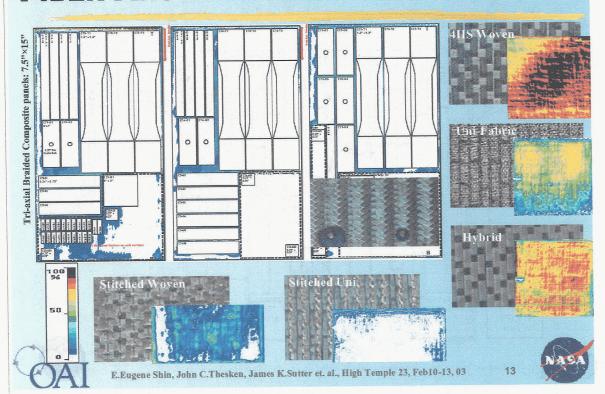
	Endcap	Dimethyl Ester	Diamine	Repeat Unit(n)	
Molar Ratio	2	n	n+1		
HFPE	C=C OCH ₃	CH ₈ O CF ₃ CF ₃ OCH ₃	H ₂ N—NH ₂	9	
	PEPE	HFDE	p-PDA		
PMR-II-50	OCH ₃	CH ₈ O CF ₃ CF ₃ O OCH ₃	H ₂ N-\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	9	
	NE	HFDE	p-PDA		

Ref: 1. Kathy C. Chuang, Joseph E. Waters, Int'l SAMPE Symposium, 40, 1113 (1995)
 2. Kathy C. Chuang, Demetrio S. Papadopulous, Cory P. Arendt, Int'l SAMPE Symposium, 47, 1175 (2002)





FIBER ARCHITECTURE: TEST PANELS



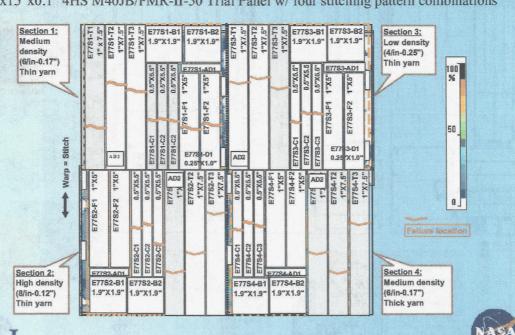
STITCHING OPTIMIZATION: VARIATION

- ☐ Stitching --- Excellent blistering stopper, but at the expense of the in-plane mechanical properties?
 - Stitching Options with 4HS Woven Fabric
 - Stitch density; 4:6:8 stitches per inch
 - ❖Stitch-line spacing; 0.12": 0.17": 0.25"
 - Stitching yarn size (S2 glass); thin (150 1/0): thick (150 1/2)
 - Properties Evaluated
 - Tension, Compression, and Flexure
 - ❖Void content, FVF, Ta, Td, CoTE
 - Hygrothermal Blistering Test
 - > Fully saturated
 - > 20 & 50 oC/min heating





STITCHING OPTIMIZATION: TEST MATRIX 15"x15"x0.1" 4HS M40JB/PMR-II-50 Trial Panel w/ four stitching pattern combinations



STITCHING OPTIMIZATION: TEST RESULTS

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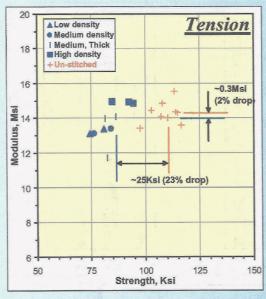
Stitch Pattern	FVF, %
Low Density Thin Yarn; 4 stitches/in; 0.25" spacing	53 ± 0.4
Medium Density 1 Thin Yarn; 6 stitches/in; 0.17" spacing	57 ± 0.5
Medium Density 2 Thick Yarn; 6 stitches/in; 0.17" spacing	60 ± 0.4
High Density Thin Yarn; 8 stitches/in; 0.12" spacing	59 ± 1.1

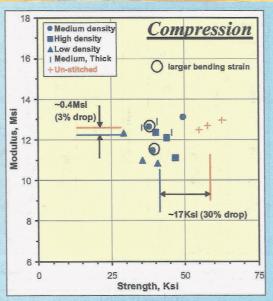




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STITCHING OPTIMIZATION: TEST RESULTS





Note: 1. Stitched panels by SaRTM @ 300psi vs. Un-stitched by Hot-press @ 500psi 2. Stitched samples tested @ 0.5in/min vs. Un-stitched @ 0.05in/min

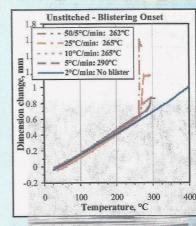


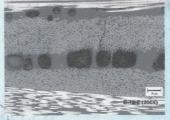
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STITCHING OPTIMIZATION: TEST RESULTS





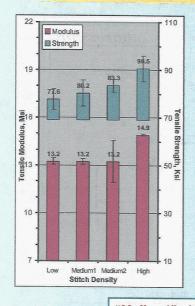
Blistering Resistance

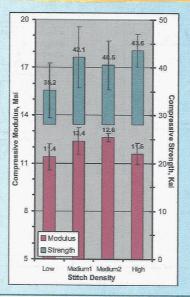
Stitch	Void Cont. %	Moisture	Blister Onset, °C		
Density		Uptake, %	Rate 1*	Rate 2**	
Un-stitched	2.3 ± 0.4	1.47	262	N/A	
Low	5.8 ± 0.1	1.74	None	280	
Medium 1	4.9 ± 1.2	1.74	None	None	
Medium 2; thick yarn	4.6 ± 0.1	1.64	None	310	
High	3.6 ± 0.5	1.63	None	N/A	

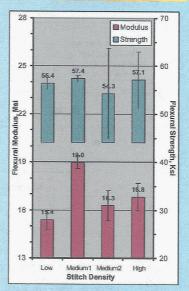
- * Heating Rate 1: 50°C/min to 250°C ⇒ 5°C/min to 400°C
- ** Heating Rate 2: 50°C/min to 400°C



STITCHING OPTIMIZATION: TEST RESULTS







"Medium 1" w/ thin yarn was selected for:

Better Compressive & Flexural Performance, and Blistering Resistance



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STITCHING: TRANSVERSE PROPERTIES

4 M40JB Uni-fabric [0/90]₆₈/HFPE-II-52 Composite Panel w/ Boeing Stitching (40 penetration/in²; 5 stitches/in − 1/8 spacing by Lock-stitch w/ fiber glass yarn)

Typical Cross-Section normal to Stitch Direction



Transverse Direction

Stitch Lines

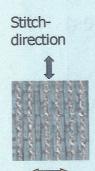
~ 0.11" Thick; 4.0±0.5% Void Content; 58±1.5% F.V.F



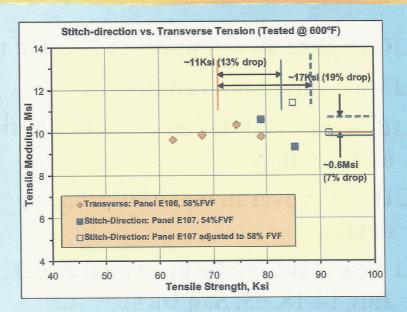




STITCHING: TRANSVERSE PROPERTIES



Transverse





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SUMMARY & CONCLUSIONS

- ☐ Studied six representative fiber architectures, optimized design and process, completed test panel fabrication and test specimen preparation
 - Testing underway...
- ☐ Selected the medium density w/ thin yarn as the optimum stitching pattern based on mechanical properties and blistering performance,
- Resulted in-plane property degradation of stitched panel; 2~3% in modulus but 20~30% in strength in both tension and compression,
- ☐ Transverse property degradation in stitched panel; 15~20% tensile strength drop due to:
 - array formation of the stitch-induced damage normal to transverse direction?





CONTINUING WORK PLANS

- □ Complete all composite evaluation tests...
- ■Micro-mechanics analysis...
- ☐ Best material-design-process selection and optimization
- **□** Develop overall material-property database
- New results to be presented at ICCM-14, July 14-18, 03, San Diego, CA.



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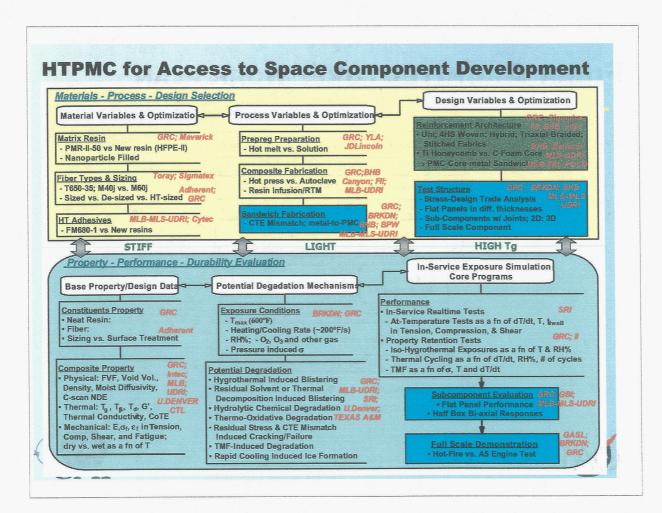


ACKNOWLEDGEMENT

- ■Maverick Corp.; PMR-II-50 resin
- □ Joe Lavelle & Tim Ubienski; test specimen preparation for stitch optimization
- □ David Hull, GRC; OM microscopy







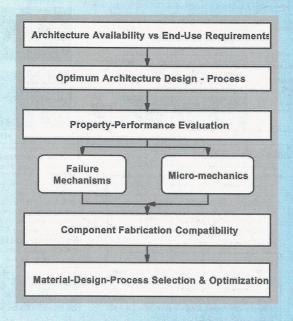
FIBER ARCHITECTURE: OBJECTIVES

- Evaluate PMC materials and generate database as a function of fiber reinforcement architecture for temperature-moisture-stress-high heating rate Aeropropulsion applications
- Optimize design and fabrication processes





FIBER ARCHITECTURE: WORK PLAN





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FIBER ARCHITECTURE: TEST MATRIX

TES1	TYPE	CO	MPOSITE PANEL T			THE RESERVE OF THE PARTY OF THE	THE RESIDENCE OF THE PARTY OF T	
PROPERTIES CONDITIONS			UNI-TAPE	UNI-WOVEN	TRIAXIAL		STITCHED	
ROPERTIES	Dry RT	FABRIC	CROSS-PLY	HYBRID	BRAID	UNI-TAPE	4HS WOVEN	
Compression	Dry T _{max} (600°F)		04 1	• 8-ply fabric +				
(A repeats) -	Wet T _{max} (600°F)	- 12-ply fabric; - [0,90,90,0,0,90] ₁₈ 0.1" TH	• 24-ply uni; [0,90,90,0,90,0,0, 90,0,90,90,0] ₁₆ ~0.1" TH	8-ply uni; [0,90,0,90,0,0,0,9 0,90], _s ~0.1" TH		100 -/- 2 1	08 g/m ² FAW per layer 6K M40J C-fiber	
Open Hole	Dry RT				CONTRACTOR STATE			
Comp/Northrop	Dry T (600°F)					w/6K M40J		
3 repeats)	Wet T _{max} (600°F)				_			
	Dry RT	• 2-; [0dia, 0.02"TH	· 4-; [0,90] ₁₈ , 0.02"	• 8/8 fabric/uni;				
Tension		• 4-;[0,90] ₁₈ , 0.033"	• 8-; [0,90,90,0] _{18.}	- 2/4 fabric/uni;				
(3 repeats)	Dry T _{max} (600°F)	• 12-ply fabric	~0.035" TH	[0,80,0]18;				
V	Wet T _{max} (600°F)	- 12-ply labric	- 24-ply uni	~0.035" TH		ent - 24-ply uni;	• 12-ply fabric; [0,90,90,0,0,90] By SaRTM	
SBS	Dry RT				to 12-ply fabric,	[0,90] _{es} ;		
(6 reneats)	Dry T _{max} (600°F)				iaunc,	HFPE-II-52		
	Wet T _{max} (600°F)				By SaRTI		~0.11" TH	
In-plane Shear	Dry RT				~0.1" TH			
	Dry T _{max} (600°F)	• 12-ply fabric	• 24-ply uni	• 8-ply fabric + 8-ply uni				
(3 repeats)	Wet T _{max} (600°F)							
DMA	IRT to 500°C							
TMA (both X & Z)			0,0,1,s, 0.052"TH					
TGA	RT to 800°C	CARSON CARDON PROPERTY.						
Thermal Cond.	RT to Tmax (600°F)	- 8-; [0 ₁ ,90	0,90,0 ₀ 1 ₁₅ , 0.065"TH					
Moisture Diff.	RT to 80°F	2, 4, 6, 8, & 12-ply		• 8/8 fabric/uni				
Blistering	2"×2" coupon	fabric		• 2/4 fabric/uni				
Fully Saturated)	12"×12" panel							
Hygrothermal Rap (w/ 12"×12" panel	oid heat-up Cycle	Selected Architectur	e Systems Only					

DAI

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